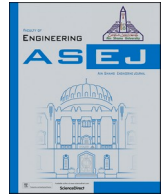




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Solar radiation and Lorentz force effects on Reiner-Rivlin nanofluid flow over a spinning disk with activation energy

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ABSTRACT

The enhancement of thermal efficiency in energy conversion processes holds great importance in numerous sectors. The addition of nanoparticles into working fluid helps in the attainment of improved thermal efficiency. Hence, the main objective of the present study is to examine the irreversibility of the flow of magnetized Reiner Rivlin nano-fluid over a stretchable rotating disk. The electrically conducted fluid takes into account in the presence of the induced electric field. The energy expression is characterized by exothermic or endothermic reactions with activation energy, radiation, Joule heating, dissipation effects and these phenomena are uniqueness of the current work. The disk surface is subjected to slip factor and suction/injection conditions. Impacts of random and thermophoresis diffusions are considered and investigated. The entropy rate is also incorporated. The system of ordinary differential equations (ODEs) is converted through the appropriate selection of variables. The ND-solve technique is utilized to approximate solutions. The physical explanation of the flow variables concerning velocity, thermal field and entropy optimization is provided. The computational results pertaining to Sherwood number, skin friction, and temperature gradient are discussed. Enhanced entropy generation occurs as the numeric values of the electric parameter, radiation parameter and Brinkman number increase. Therefore, motivated by the above practical application to attempt the present study.

1. Introduction

Nanomaterials has a variety of applications in many areas, including cooling towers, tumor therapy, microelectronics cooling, industrial cooling, imaging, heating of home appliances, development of new types of fuels, nanotechnology is used in human lives because of its importance and utilization in many sectors like in electronics, biomedical science, cancer treatment, agriculture, and medical sciences (nano robots are injected into the blood stream for recovery and repairing processes) [1]. Improvement of cutting-edge performance of isolated thermal systems for thermal carriage has become increasingly popular in recent years. It is due to its numerous uses in paper making industry, medical equipment, medicine production, heat exchangers, thermal power stations, thermal transport, microelectronics, and some relevant other fields. There are several methods for improving the efficiency of

heat transfer of base liquid (air, water, kerosene oil, propylene and ethylene glycols) etc. Thermal heat transfer can also be improved by enhancing the heat transmission of the base liquid (working materials).

For this nanoparticles can be inserted to improve thermal conductivity of base liquids [2]. Nano sheets, nanowires, nanotubes, nanocones, nan-rods, nanoparticles, and nanofluids such as ethyl-glycol, oil, and water are examples of nanoscale materials. Drug delivery, protein engineering, cancer diagnostics and treatment, photodynamic treatment, biotherapy, shedding new light on cells, molecular motors such as kinesin surgery, and neuro electronic interfaces are just a few of the applications for nanofluids [3]. Choi and Eastman explained how nanoparticles distributed in a base liquid can be used in various thermal frameworks to improve the rate of heat exchange [4]. In the past few decades, nanoparticles have been utilized as an attractive agent in the production of fluids to improve heat transfer in automation technology [5]. The different applications and properties of nanofluid were

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Nomenclature

$u, v, w (ms^{-1})$	Velocity components	Br	Brinkman number
L	Diffusion variable	Nt	Thermophoresis variable
δ_{ij}	Kronecker symbol	$r, \varphi, z(m)$	Cylindrical coordinates
μ_c	Coefficient of cross viscosity	L_1	Velocity slip factor
$T_\infty(K)$	Ambient temperature	$C_{f,r}$	Coefficient of Skin friction
$T(K)$	Fluid temperature	j_w	Mass flux
M	Magnetic parameter	$q_w(kgs^{-3})$	Heat flux
C_w	Wall concentrations	λ_1	Exothermic reaction parameter
τ_{ij}	Cauchy stress tensor	$p(pa)$	Pressure
Ec	Eckert number	c_p	Specific heat
$k_f(kgm^{-1}s^{-3})$	Thermal conductivity	μ_f	Dynamic viscosity
$\nu_f(m^2s^{-1})$	Kinematic viscosity	e_{ij}	Deformation rate tensor
k_r^2	Rate of reaction	$T_w(K)$	Wall temperature
B_T	Biot number due to temperature.	$k^*(m^{-1})$	Coefficient of mean absorption
Re_r	Local Reynolds number	B_c	Biot number due to concentration.
σ^*	Stephan-Boltzmann constant	D_T	Thermophoresis coefficient
Nu_r	Nusselt number	$\rho_f(kgm^{-3})$	Density
$f'(\eta)$	Dimensionless radial velocity	β	Reiner-Rivlin fluid parameter
(ρc_p)	Fluid heat capacity	Pr	Prandtl number
Sh_r	Sherwood number	Sc	Schmidt number
D_B	Brownian motion parameter	α_2	Concentration difference variable
A	Stretching variable	$C_{m,r}$	Moment coefficient
Rd	Radiation variable	u_w	Stretching velocity
E_a	Activation energy	σ_1	Reaction parameter
γ	Chemical reaction variable	N_G	Rate of entropy generation
α_1	Temperature difference variable	Nb	Brownian diffusion parameter
h_c	Coefficient of mass transfer	h_f	Coefficient of heat transfer
E_1	Electric parameter	δ	Temperature ratio parameter
		β_1	Suction/injection parameter

discovered by many others researchers by taking the novel approach and tried something new [6–28]. It is also shown that spherical nanoparticles contribute less heat exchange, but platelet nanoparticles deliver higher heat transfer [29]. Ullah et al [30] investigated the use of an infinite porous disk to communicate the Marangoni convection flow of hybrid nanomaterials.

In 1889, a Swedish scientist named Arrhenius coined the term activation energy, which can be defined as the Minimum quantity of energy essential to activate a chemical process. The Arrhenius equation can be used to calculate the quantity of activation energy [31]. The minimal energy acquired by the atoms or molecules to activate the chemical reaction is denoted by E_a , which is measured in KJ/mol. Bestman [32] published the earliest paper on activation energy in binary chemical reactions. Awad et al. [33] investigated the effects of activation energy and binary chemical process in a viscous rotating flow. Ullah et al. [34] examined numerically the flow of second-grade nanoliquid with the Arrhenius activation energy and binary chemical reaction in a spongy media. Examples of activation energy and chemical reactions comprise of thermal oil recovery, food processing, chemical energy, geothermal engineering, water emulsion and nuclear reactors [35]. The implications of activation energy in melting conditions on nanofluid flow are investigated theoretically [36]. Ullah et al. [37] investigated the combined heat source and features of zero mass flux on magnetic nanofluid flow by radial disk with the use of activation energy.

Entropy is a term that refers to the unpredictability or disorder of a system or environment. The relation of reversible heat to temperature is also used to calculate entropy. The performance of thermal machines such as air conditioners, heat pumps, and energy plants is measured due to entropy generation. Bejan [38] for the first time addressed the entropy generation problem. Alkanhal et al. [39] investigate entropy generation for magnetohydrodynamic flow of nanofluids with

convective heat transfer. Li et al. [40] used helical twisted tapes to demonstrate entropy analysis on nanofluids with convective heat transfer. The generation of entropy can be used as a criteria for evaluating the performance of engineering devices [41]. Dormohammadi et al. [42] investigated the effects of entropy generation optimization on nanomaterial convective flow with heat flux. Rashidi et al. [43] investigated the generation of entropy in 3rd-grade fluid. K. Loganathan et al. [3] used the CCHF model to investigate the impact of 3rd-grade nanofluid flow across a convective surface of inclined magnetic field impacts on entropy formation of 3rd-grade nanofluid across the convective surface. Micro polar nanofluid free convection and entropy generation are achieved using an inclined I-shaped cage with two heated cylinders [44].

Fortified from of all the above theoretical and mathematical work discussed in literature regarding nanofluid flow, heat transfer exploration and entropy analysis to a diverse geometry. Our objective here is to consider the significances of nanofluid flow, activation energy with exothermic/endothermic reaction and entropy generation in the presence of radiation, Joule heating and Lorentz force. The novelty structure of this proposed efforts are as follows.

- To model the entropy analysis in Reiner-Rivlin nanofluid past a rotating disk.
- An Exothermic/endothermic reaction along with activation energy which start the chemical reaction is taken detail analysis of heat transfer.
- The slip factor and convective conditions are imposed at the boundary.
- To see the significant changes in velocity gradient and rate of heat transfer against involve parameters.

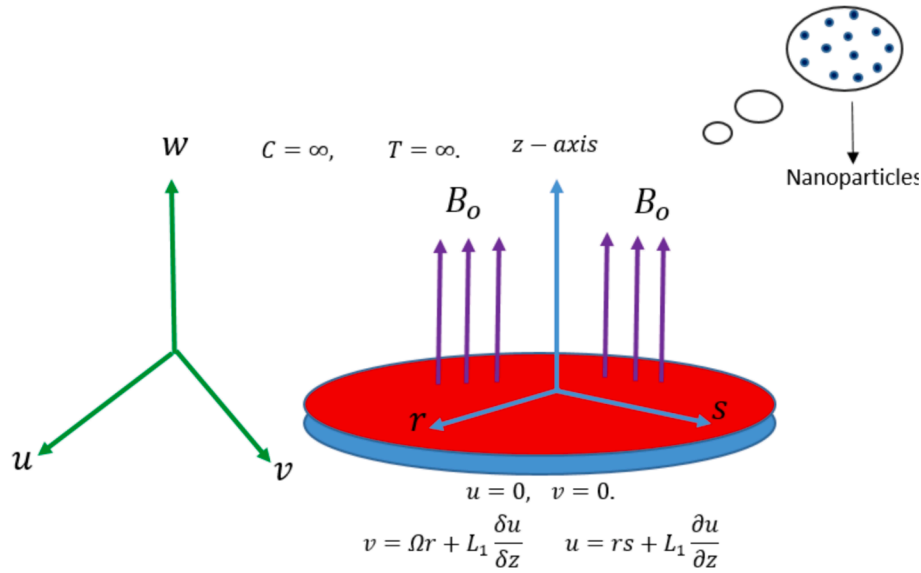


Fig. 1. Flow configuration.

- To inspect the variations in thermal analysis in the presence of exothermic reaction.
- To show the influence of the rate of heat energy with variation in various parameters.
- To study the physical behavior of entropy generation through rise in different influential variables.

System of ordinary differential equation have been obtained through applying suitable transformation technique. The Modeled system have been attempted through NDSolve method. Various variables on concentration, and temperature and entropy optimization are entertained through graphs and tables. The remarkable properties of this theoretical study have potential applications in various fields, including material science, purification technologies, optics, electricity, aerospace industry, and beyond. Particularly in the aerospace sector, this assistance can be instrumental in reducing weight, achieving satellite weight reduction, providing lightning protection for aircraft, and more.

2. Mathematical modeling

In this section the 3D steady flow of Reiner-Rivlin nanofluid by a stretchable rotating disk is considered. The disk is rotating with velocity \$(\Omega r)\$. Heat equation modeled through dissipations, radiation, random and thermophoresis diffusion, are considered. Electric and magnetic fields are added for further inspection. To study irreversibility analysis, the 1st and 2nd law of thermodynamics are implemented. The reaction rate is also taken into account. Cylindrical coordinates \$(r, \varphi, z)\$ are used to model the governing equation. Let \$u_w = rs\$ is considered as stretching velocity with stretching rate constant \$(s > 0)\$. Furthermore, suction/injection and slip effects are included for heat transfer and flow investigation. In light of the preceding considerations, the flow governing expressions governing expressions [45] are: (See Fig. 1)

$$\tau_{ij} = \mu_f e_{ij} - p \delta_{ij} + \mu_c e_{ik} e_{kj} e_{ij}. \quad (1)$$

In the above equation the \$p\$ indicates pressure, \$\mu_f\$ dynamic velocity, \$e_{ij}\$ the deformation rate tensor and \$\delta_{ij}\$ the kronecker delta.

$$\frac{\partial u}{\partial r} + \frac{u}{r} + \frac{\partial w}{\partial z} = 0, \quad (2)$$

$$u \frac{\partial u}{\partial r} - \frac{v^2}{r} + w \frac{\partial u}{\partial z} = \nu_f \frac{\partial^2 u}{\partial z^2} + \frac{\mu_c}{\rho_f} \left(\frac{\partial^2 v}{\partial z^2} \left(\frac{\partial u}{\partial r} - \frac{v}{r} \right) + \frac{\partial v}{\partial z} \left(\frac{\partial^2 v}{\partial r \partial z} - \frac{1}{r} \frac{\partial v}{\partial z} \right) + 2 \frac{\partial u \partial^2 w}{\partial z \partial z^2} + \frac{1}{r} \left(\left(\frac{\partial u}{\partial z} \right)^2 - \left(\frac{\partial v}{\partial z} \right)^2 \right) \right) + \frac{\delta}{\rho_f} (E_o B_o - B_o^2 v) \quad (3)$$

$$u \frac{\partial u}{\partial r} + \frac{uv}{r} + w \frac{\partial u}{\partial z} = \nu_f \frac{\partial^2 v}{\partial z^2} + \frac{\mu_c}{\rho_f} \left(\frac{\partial^2 u}{\partial z^2} \left(\frac{\partial v}{\partial r} - \frac{v}{r} \right) + \frac{\partial u}{\partial z} \left(\frac{\partial^2 v}{\partial r \partial z} - \frac{1}{r} \frac{\partial v}{\partial z} \right) + 2 \frac{u \partial^2 v}{r \partial z^2} + 2 \frac{\partial^2 u}{r \partial z^2} \left(\left(\frac{\partial u}{\partial z} \right)^2 - \left(\frac{\partial v}{\partial z} \right)^2 \right) \right) + \frac{\delta}{\rho_f} (E_o B_o - B_o v) \quad (4)$$

$$u \frac{\partial T}{\partial r} + w \frac{\partial T}{\partial z} = \frac{k_f}{(\rho c_p)_f} \left(1 + \frac{16 \sigma^* T_\infty^3}{3 k_f k^*} \right) \frac{\partial^2 T}{\partial z^2} + \tau \left(D_B \frac{\partial T \partial C}{\partial z \partial z} + \frac{D_T}{T_\infty} \left(\frac{\partial T}{\partial z} \right)^2 \right) + \frac{\mu_f}{(\rho c_p)_f} \left(\left(\frac{\partial u}{\partial z} \right)^2 + \left(\frac{\partial v}{\partial z} \right)^2 \right) + \beta_1 k_r^2 (C - C_\infty) \left(\frac{T}{T_\infty} \right)^m \exp \left(\frac{E_a}{\kappa T} \right) + \frac{\mu_f}{(\rho c_p)_f} \left(\frac{\partial w}{\partial z} \left(\frac{\partial v}{\partial z} \right)^2 + \frac{\partial u \partial v \partial v}{\partial z \partial z \partial r} - \frac{v \partial u \partial v}{r \partial z \partial z} + 2 \frac{u}{r} \left(\frac{\partial v}{\partial z} \right)^2 + 2 \frac{\partial u \partial u}{\partial z \partial r} \left(\frac{\partial u}{\partial z} + \frac{\partial w}{\partial z} \right) + \left(\frac{\partial u}{\partial z} + \frac{\partial w}{\partial z} \right) \left(\frac{\partial v}{\partial r} - \frac{v}{r} \right) \frac{\partial v}{\partial z} + 2 \frac{\partial u \partial w}{\partial z \partial z} \left(\frac{\partial u}{\partial z} + \frac{\partial w}{\partial z} \right) + \frac{\partial v \partial u}{\partial z \partial z} \left(\frac{\partial v}{\partial r} - \frac{v}{r} \right) + 2 \frac{\partial w}{\partial z} \left(\frac{\partial v}{\partial z} \right)^2 \right) + \frac{\delta_f}{(\rho c_p)_f} \{ (u^2 + v^2) \beta_0^2 - 2 E_0^2 \}, \quad (5)$$

$$u \frac{\partial C}{\partial r} + w \frac{\partial C}{\partial z} = D_B \frac{\partial^2 C}{\partial z^2} + \frac{D_T}{T_\infty} \frac{\partial^2 T}{\partial z^2} - k_r^2 (C - C_\infty) \left(\frac{T}{T_\infty} \right)^m \exp \left(\frac{-E_a}{\kappa T} \right), \quad (6)$$

with conditions

$$\left. \begin{aligned} u &= sr + L_1 \frac{\partial u}{\partial z}, & v &= \Omega r + L_1 \frac{\partial v}{\partial z}, & w &= -w_0, \\ k \frac{\partial T}{\partial z} &= -h_f(T_f - T), & -D_B \frac{\partial C}{\partial z} &= h_c(C_f - C), & \text{at } z &= 0, \\ u &\rightarrow 0, v \rightarrow 0, C \rightarrow C_\infty, T \rightarrow T_\infty, & \text{as } z &\rightarrow \infty. \end{aligned} \right\} \quad (7)$$

Utilizing

$$\left. \begin{aligned} u &= r\Omega f'(\eta), & w &= 2\sqrt{\Omega\nu_f}f(\eta), & v &= r\Omega g(\eta), \\ \theta(\eta) &= \frac{(T - T_\infty)}{(T_f - T_\infty)}, & \phi(\eta) &= \frac{(C - C_\infty)}{(C_f - C_\infty)}, & \eta &= \sqrt{\frac{\Omega}{\nu_f}}z, \end{aligned} \right\} \quad (8)$$

Eq. (1) is satisfied identically whereas other expressions are

$$f''' - f'^2 + 2ff'' + g^2 + \beta(ff''^2 - 2f'f'' - g'^2) + M(E_1 - f') = 0, \quad (9)$$

$$g'' - 2fg' + 2f'g + 2b(f''g' + f'g'') + M(E_1 - g) = 0, \quad (10)$$

$$\left. \begin{aligned} (1 + Rd)\theta'' + Prf'\theta' + Br(1 - 3\beta f')(f'^2 + g'^2) + PrNb\theta'\phi' + PrNt\theta'^2 \\ + \lambda_1\sigma_1(1 + \delta\theta)^m \exp\left(-\frac{E_a}{(1 + \delta\theta)}\right) + MBr(f'^2 + g'^2 - E_1^2) = 0, \end{aligned} \right\} \quad (11)$$

$$\phi'' + Scf'\phi' + \frac{Nt}{Nb}\theta'' - Sc\sigma_1(1 + \delta\theta)^m \exp\left(-\frac{E_a}{(1 + \delta\theta)}\right) = 0, \quad (12)$$

$$\left. \begin{aligned} f'(0) &= \gamma + \gamma f''(0), & f(0) &= \beta_1, & g(0) &= 1 + \gamma_s g'(0), \\ \theta'(0) &= -B_T(1 - \theta(0)), & \phi'(0) &= -B_c(1 - \phi(0)), \\ f'(\infty) &= \theta(\infty) = \phi(\infty) = 0. \end{aligned} \right\} \quad (13)$$

Here the dimensionless parameter are defined as

$$\left. \begin{aligned} Rd &= \frac{16\sigma^* T_\infty^3}{3k_f k^*}, & \beta &= \frac{\mu_c \Omega}{\mu_f}, & \gamma &= \frac{s}{\Omega}, & Ec &= \frac{u_w^2}{c_p(T_f - T_\infty)}, & Nt &= \frac{\tau D_T(T_f - T_\infty)}{T_\infty \nu_f} \\ Pr &= \frac{\mu_f c_p}{k_f}, & Nb &= \frac{\tau D_B(C_f - C_\infty)}{\nu_f}, & Br &= PrEc, & Sc &= \frac{\nu_f}{D_B}, & \beta_2 &= \frac{w_0}{\sqrt{2\Omega\nu_f}} \\ E_1 &= \frac{E_0}{\gamma\Omega B_0}, & M &= \frac{\sigma B_0^2}{\rho_f \Omega}, & \lambda_1 &= \frac{B_1 C_\infty}{(\rho c_p)_f(T_f - T_\infty)}, & \delta &= \frac{T_f - T_\infty}{T_\infty}, & E &= \frac{E_a}{k_f T_\infty} \\ \sigma_1 &= \frac{K_r^2}{s}, & B_c &= \frac{h_f}{D_b} \sqrt{\frac{\nu_f}{2\Omega}}, & B_r &= \frac{h_c}{k_f} \sqrt{\frac{\nu_f}{2\Omega}}, & Re &= \frac{r^2 \Omega}{\nu_f}, & \gamma_s &= Lu_f \sqrt{\frac{2\Omega}{\nu_f}} \end{aligned} \right\} \quad (14)$$

In the above equations, Eq. (2) is based on the conservation of mass as continuity equation. Eq. (3) shows momentum equation, its L.H.S shows internal forces, where the 1st term in the R.H.S is surface force and 2nd term as body forces (induced electric and magnetic force), the 5th equation is energy equation, the L.H.S is total internal energy, whereas, 1st term in R.H.S is thermal radiation, 2nd term is Fourier's law of heat flux, 3rd term is viscous dissipation, 4th term is exothermic, endothermic energy. There is activation energy in the 6th equation. Eq. (7) has velocity slip, angular velocity, convective boundary condition for heat and mass diffusion.

Where Rd radiation parameter, β suction /injection parameter, γ stretching variable, Eckert number Ec , Nt thermophoretic variable, Pr

Prandtl number, Nb Brownian diffusion variable, Br Brinkman number, Sc Schmidt number, β_2 suction number, E_1 the electric parameter, M magnetic parameter, λ_1 exothermic reaction parameter, δ temperature ratio parameter, T_f temperature of heated fluid, β_0 is the strength of the magnetic field applied, L diffusion parameter, γ_s slip parameter, σ_1 is the reaction parameter, B_c and B_T denotes Biot number due to concentration and and temperature respectively.

3. Entropy modeling

Mathematical expression for entropy is

$$\left. \begin{aligned} S_G &= \frac{k_f}{T_\infty^2} \left(1 + \frac{16\sigma^* T_\infty^3}{3k_f k^*} \right) \left(\frac{\partial T}{\partial z} \right)^2 + \frac{\mu_f}{T_\infty} \left(\left(\frac{\partial u}{\partial z} \right)^2 + \left(\frac{\partial v}{\partial z} \right)^2 \right) \\ &+ \frac{\mu_f}{T_\infty} \left(\begin{aligned} &\frac{\partial w}{\partial z} \left(\frac{\partial v}{\partial z} \right)^2 + \frac{\partial v \partial u \partial v}{\partial z \partial z \partial z} - \frac{\nu \partial u \partial v}{r \partial z \partial z} 2 \frac{u}{r} \left(\frac{\partial v}{\partial z} \right)^2 \\ &2 \frac{\partial u \partial u}{\partial z \partial r} \left(\frac{\partial w}{\partial z} + \frac{\partial u}{\partial z} \right) + \left(\frac{\partial w}{\partial z} + \frac{\partial u}{\partial z} \right) \left(\frac{\partial w}{\partial z} - \frac{\nu}{r} \right) \frac{\partial v}{\partial z} \\ &+ 2 \frac{\partial w \partial u}{\partial z \partial z} \left(\frac{\partial w}{\partial z} + \frac{\partial u}{\partial z} \right) + \frac{\partial u \partial v}{\partial z \partial z} \left(\frac{\partial v}{\partial z} - \frac{\nu}{r} \right) + 2 \frac{\partial w}{\partial z} \left(\frac{\partial v}{\partial z} \right)^2 \\ &\frac{R_D}{T_\infty} \left(\frac{\partial C \partial T}{\partial z \partial z} \right) + \frac{R_D}{T_\infty} \left(\frac{\partial C}{\partial z} \right)^2 \end{aligned} \right) \quad (15) \end{aligned}$$

Using eq. (8), the above expression reduces to

$$\left. \begin{aligned} S_G &= \alpha_1(1 + Rd)\theta'^2 + Br(1 - 3\beta f')(f'^2 + g'^2) + \frac{\alpha_1}{\alpha_2} g\phi'^2 + L\theta'\phi' + \\ &L \frac{\alpha_1}{\alpha_2} \phi'^2 + M(f'^2 + g'^2 - E_1^2). \end{aligned} \right\} \quad (16)$$

The dimensionless variables are

$$\left. \begin{aligned} S_G &= \frac{S_G \nu_f T_\infty}{k_f \Omega (T_f - T_\infty)}, & L &= \frac{R_D (C_f - C_\infty) \nu_f T_\infty}{k_f}, & \alpha_1 &= \frac{(T_f - T_\infty)}{T_\infty}, & \alpha_2 &= \frac{(C_f - C_\infty)}{C_\infty} \end{aligned} \right\} \quad (17)$$

4. Physical quantities

The physical quantities i.e. moment coefficient is defined as

$$C_{m,r} = \frac{T_r}{\rho_f \Omega^2 r^5}, \quad (18)$$

where T_r specifies torque of rotating disk and is given by

$$T_r = r_0 \tau_{z\phi} 2\pi r^2 dr = \frac{\pi}{2} \rho_f \Omega \sqrt{\nu_f \Omega} (1 - 2\beta A) r^4 g'(0), \quad (19)$$

$$Re_f^{\frac{1}{2}} C_{m,r} = \frac{\pi}{2} (1 - 2A\beta) g'(0). \quad (20)$$

Table 1

Comparative analysis of present results, when $M = E_1 = \gamma = \beta_1 = \gamma_s = L_1 = \delta = B_T = B_C = \lambda_1 = 0, \beta = 0.2, Nt = 0.5, s = 0.1, Pr = 3, Rd = 0.1, Nb = 0.5, Br = 0.5, \sigma = 0, m_1 = 2, E_a = 1, Sc = 3, \sigma_1 = 0.2, \sigma_2 = 1$, with the Sadiq and Hayat [31].

Sadiq and Hayat [34]					Present result	
Nb	Nt	Sc	Nu_r	Sh_r	Nu_r	Sh_r
0.6	0.5	0.5	0.156353	0.359172	0.156342	0.359201
0.8			0.121314	0.383214	0.121311	0.383232
1.2			0.091232	0.434652	0.091227	0.434644
0.6	0.2	0.5	0.137351	0.314951	0.137348	0.314,936
	0.6		0.118341	0.278961	0.118339	0.278923
	1.0		0.084591	0.257351	0.084588	0.257344
	0.5	0.5	0.234653	0.354950	0.234647	0.354946
		0.7	0.197563	0.393560	0.197571	0.393572
		0.9	0.156573	0.457571	0.156498	0.457562

Skin friction is expressed as

$$C_{f,r} = \frac{\tau_{rz}}{\rho_f(r\Omega)^2}, \tag{21}$$

the dimensionless form is

$$Re_r^{\frac{1}{2}} C_{f,r} = f''(0)(1 - 2A\beta). \tag{22}$$

Nusselt and Sherwood numbers are defined as follow

$$Nu_r = \frac{r q_w}{k_f(T_w - T_\infty)}, Sh_r = \frac{r j_w}{D_\beta(C_w - C_\infty)}. \tag{23}$$

In dimensionless expression is

$$Re_r^{\frac{1}{2}} Sh_r = -\phi'(0), Re_r^{\frac{1}{2}} Nu_r = -(1 + Rd)\theta'(0), \tag{24}$$

the disk pumping efficiency is given by

$$Q = R_0 - 2\pi r dr(w(\infty)) = 2\Omega \sqrt{\nu_f} \Omega \pi R^2 f(\infty). \tag{25}$$

5. Method of solution and validation: –

The governing problem is modeled as non-linear system. Consequently, its exact solution is not possible to obtain. Therefore, an approximated solution can be obtained through different analytical and numerical techniques. Here in the current problem, NDSolve [46,47] based shooting technique is implemented to simulate the results in tabular and graphical forms. This technique is stable unconditionally and attains exceptional accuracy, moreover it provides outstanding results in less CPU time and evade lengthy expressions. Table. 1 depicts the comparative scrutiny with Sadiq and Hayat [47]. It is observed that current and existing outcomes manifest good match.

6. Graphical results

Here main emphasis of this portion is to inspect the behavior of significant variables on temperature, entropy rate and concentration. Computational outcomes of Nusselt, Sherwood numbers and skin friction are explored in tabular form. The fixed values of the corresponding parameters are considered as $M = 0.5, \beta = 0.2, E_1 = 0.1, \gamma = 0.5, \gamma_s = 0.1, Pr = 4, Rd = 0.1, Nt = 0.5, Nb = 0.5, Br = 0.5, \lambda_1 = 0.001, \delta = 0, m_1 = 1, E_a = 1, Sc = 3, \sigma_1 = 3, B_T = 1, B_C = 0.2$.

6.1. Variation in temperature

Figs. 2 – 4 are designed for temperature against different variables. The fixed values of the concerning parameters are considered as $M = 0.5, \beta = 0.2, E_1 = 0.1, \gamma = 0.5, \gamma_s, s = 0.1, Pr = 3, Rd = 0.1, Nt = 0.5, Nb = 0.5, Br = 0.5, \lambda_1 = 0.001, \delta = 0.2, m_1 = 2, E_a = 1, Sc = 3, \sigma_1 = 0.2, B_T = 1, B_C = 0.2$. Behaviors of temperature θ is portrayed in Fig. 2a. Here it is investigated that larger value of temperature ratio parameter δ decay the temperature. Fig. 2b labels that for higher activation energy E_a the liquid temperature $\theta(\eta)$ improves. Physically, an enhancement in E_a correspond to increase in energetic nanoparticles possessing energies greater or equal to E_a , which improves the temperature. The variation in $\theta(\eta)$ against λ_1 is depicted in Fig. 3a, it indicates that temperature is higher for higher λ_1 . In fact, higher λ_1 provides more heat to the

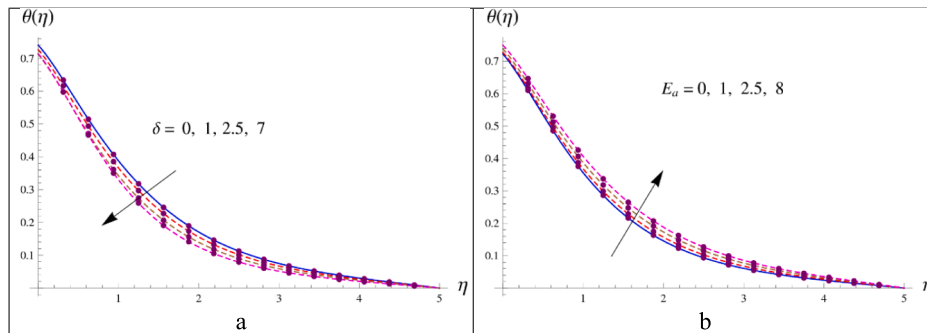


Fig. 2. (a, b) Temperature $\theta(\eta)$ for δ and E_a .

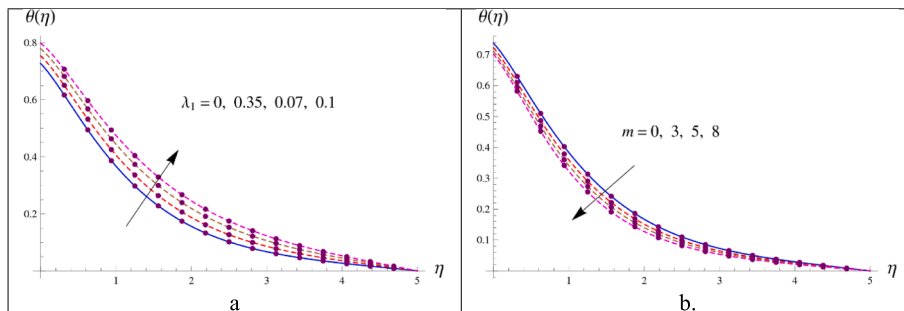


Fig. 3. (a, b) Temperature $\theta(\eta)$ for λ_1 and m .

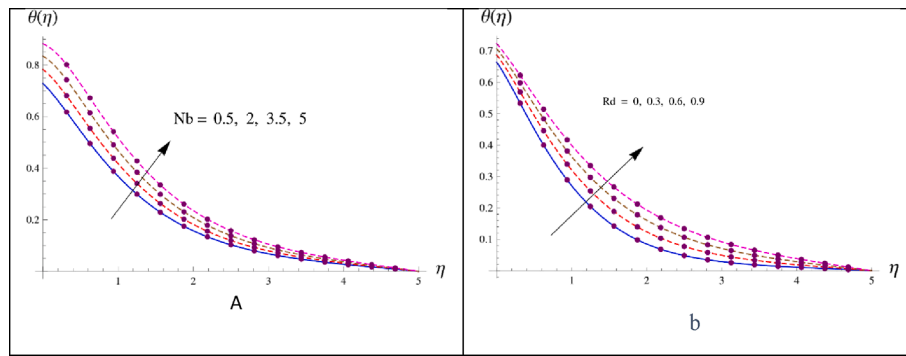


Fig. 4. (a, b) Temperature $\theta(\eta)$ for Nb and Rd .

operating liquid due to exothermic reaction. Thus $\theta(\eta)$ enhances. For higher values of fitted rate constant m a decreasing effect in liquid temperature is noticed, which is drawn in Fig. 3b. Features of $\theta(\eta)$ through variation in Nb is designed in Fig. 4a. Here temperature is significantly rises for large Nb . The rate of Brownian motion of nanoparticles increases in this case, and the consequent disorder in particle motion creates kinetic energy in nanoparticle and improves the thermal behavior of the liquid. The temperature variation via radiation parameter Rd is depicted in Fig. 4b. Physically, a reduction in the coefficient of mean absorption leads to a rise in thermal flux. As a result, temperature distribution is enhanced.

6.2. Variation in concentration

Figs. 5 and 6 are sketched to examine the behavior of concentration against numerous parameters with fixed values $M = 0.5, \beta = 0.2, E_1 = 0.1, \gamma = 0.5, \gamma_s = 0.1, Pr = 4, Rd = 0.1, Nt = 0.5, Nb = 0.5, Br = 0.5,$

$\lambda_1 = 0.001, \delta = 0, m_1 = 1, E_a = 1, Sc = 3, \sigma_1 = 3, B_T = 1, B_C = 0.2$. It is depicted in Fig. 5a that with the increase in temperature ratio parameter, concentration of the fluid decreases, while the same decreasing effect of concentration is recorded with the enhancement in Brownian diffusion parameter (see Fig. 5b). Infact higher values Nb , speed up the collection between particles which gradually decays concentration. The boosting effect is noticed in concentration with increasing the thermophoresis variable, which can clearly be seen in Fig. 6a. Physically thermophoresis phenomenon corresponds to extraction of nanoparticles from hotter zone towards ambient materials. As a consequence, the thermophoretic force admit nanoparticles to carry heat from the surface to the working liquids and thus concentration enhanced. Where reaction parameter implies diminishing effect on concentration sown in Fig. 6b.

6.3. Variation entropy

Figs. 7 – 8 are drawn to investigate the entropy rate against different

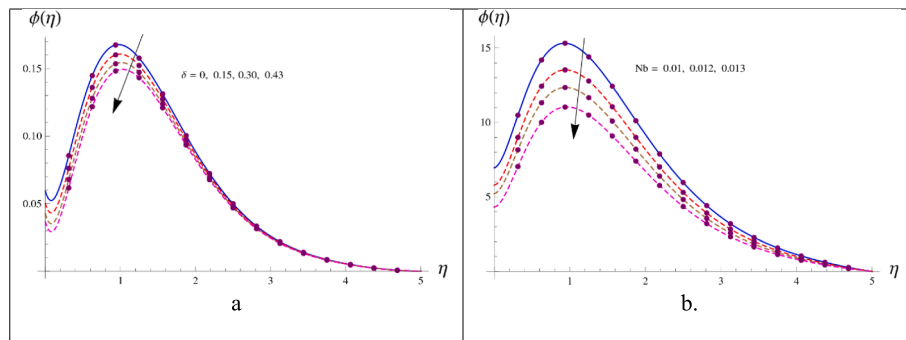


Fig. 5. (a, b). Concentration $\phi(\eta)$ for δ and Nb .

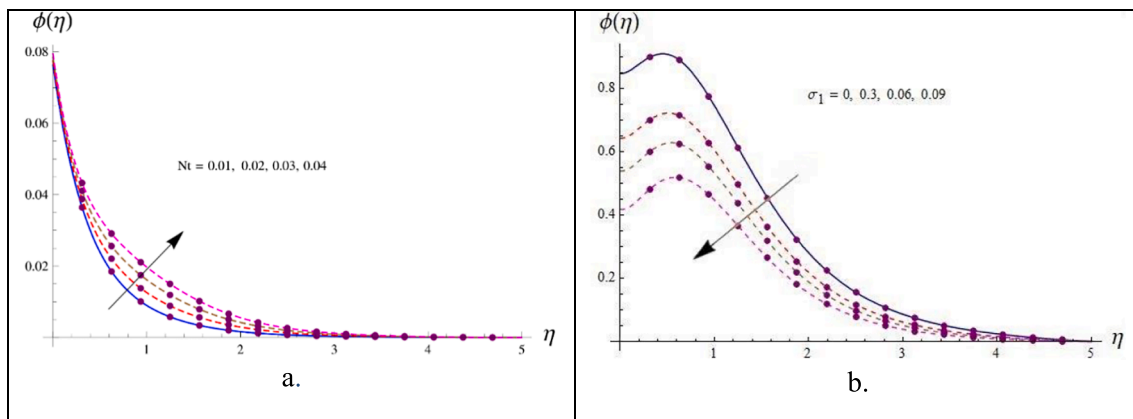


Fig. 6. (a, b). Concentration $\phi(\eta)$ for Nt and σ_1 .

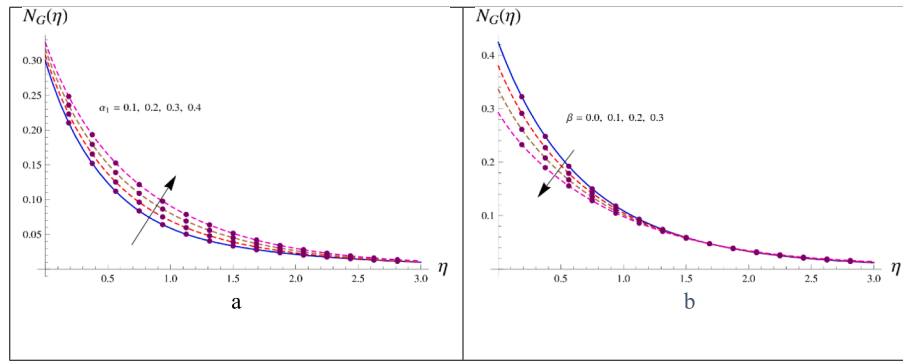


Fig. 7. (a, b) Entropy $N_G(\eta)$ for α_1 and β .

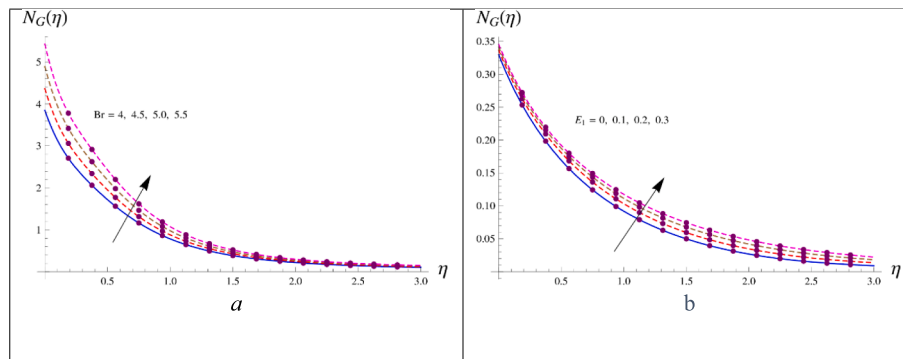


Fig. 8. (a, b) Entropy $N_G(\eta)$ for Br and E_1 .

influencing parameters. Graphical interpretation of temperature difference variable against entropy rate is displayed in Fig. 7a. An enhancement is seen in entropy rate with the increase in temperature difference parameter. Through the enhancement in Reiner-Rivlin fluid parameter, a physical change is observed in the entropy generation which can clearly be observed in Fig. 7b. Fig. 8a shows a physical description of the entropy rate as a function of Brinkman number (Br). A high Brinkman number indicates higher viscous force, which increases resistance among liquid particles. As a result, entropy generation is boosted up. Entropy generation has an increasing effect with increase in electric parameter which is displayed in Fig. 8b.

Table 2

Numerical results of $(Re_r^{-\frac{1}{2}} C_{fr})$ for $M, E_1, \beta, \beta_1, \gamma$ and γ_s .

M	E_1	β	β_1	γ	γ_s	$Re_r^{-\frac{1}{2}} C_{fr}$
0.0	0.2	0.1	0.2	0.5	0.2	0.27675
0.3						0.27700
0.6						0.27906
0.2	0.0	0.1	0.2	0.5	0.2	0.29197
	0.2					0.27695
	0.4					0.25447
0.2	0.1	0.0	0.2	0.5	0.5	0.29141
		0.1				0.27695
		0.2				0.25922
0.2	0.1	0.5	0.0	0.5	0.5	0.17425
			0.2			0.27695
			0.4			0.40126
0.2	0.1	0.1	0.2	0.5	0.5	0.27695
				0.6		0.38786
				0.7		0.50119
0.2	0.1	0.1	0.2	0.5	0.0	0.29180
					0.2	0.27700
					0.4	0.24497

6.4. Engineering interest

The influence of numerous variables such as magnetic parameter M , the electric parameter E_1 , Reiner- Rivilin fluid parameter β , suction/

Table 3

Numerical results of $(Re_r^{-\frac{1}{2}} Nu_r)$ for $Rd, Br, E_a, \lambda_1, \delta, Nt, Nb, Bt$ and E_1 .

Rd	Br	E_1	λ_1	δ	Nt	Nb	Bt	E_1	$Re_r^{-\frac{1}{2}} Nu_r$
0.0	0.5	0.1	0.001	0.2	0.5	0.2	0.1	0.2	0.32973
0.2									0.37172
0.4									0.41021
0.2	0.0	0.1	0.001	0.2	0.5	0.2	0.1	0.2	0.54000
	0.2								0.49554
	0.4								0.45091
0.2	0.1	0.1	0.001	0.2	0.5	0.2	0.1	0.2	0.42759
		0.2							0.42042
		0.3							0.41210
0.2	0.5		0.0	0.2	0.5	0.2	0.1	0.2	0.42927
			0.01						0.42195
			0.02						0.41491
0.2	0.5	0.1	0.01	0.0	0.5	0.2	0.1	0.2	0.42625
				0.2					0.42853
				0.4					0.43121
0.2	0.5	0.1	0.01	0.2	0.0	0.2	0.1	0.2	0.52983
					0.4				0.44721
					0.8				0.37681
0.2	0.5	0.1	0.01	0.2	0.5	0.1	0.1	0.2	0.43125
						0.3			0.42448
						0.6			0.41217
0.2	0.5	0.1	0.01	0.2	0.5	0.2	0.1	0.2	0.10516
							0.1		0.50157
							0.2		0.50256
0.2	0.5	0.1	0.01	0.2	0.5	0.2	0.1	0.0	0.41340
								0.1	0.42853
								0.3	0.43590

Table 4

Numerical results of $(Re_r^{-\frac{1}{2}}Sh_r)$ for $E_a, \delta_1, \delta, Bc, Nt$ and Nb .

E_a	α_1	δ	Bc	Nt	Nb	$Re_r^{-\frac{1}{2}}Sh_r$
01	0.9	0.2	0.2	0.5	0.2	0.13556
02						0.07333
03						0.01924
01	0.1	0.2	0.2	0.5	0.2	0.00497
	0.3					0.06304
	0.5					0.09643
01	0.9	0.0	0.2	0.5	0.2	0.12650
		0.3				0.13963
		0.6				0.14990
01	0.9	0.2	0.1	0.5	0.2	0.06876
			0.2			0.13556
			0.4			0.25025
01	0.9	0.2	0.2	0.0	0.2	0.17844
				0.4		0.13755
				0.6		0.13590
01	0.9	0.2	0.2	0.5	0.1	0.08080
					0.2	0.13556
					0.3	0.15144

injection parameter β_1 , chemical reaction variable γ and slip parameter γ_s on skin friction coefficient $Re_r^{-\frac{1}{2}}C_{f,r}$ is shown in Table.2. For ligger, E_1 , β , and γ_s the skin friction coefficient begins to decline, while the opposite effect can clearly be observed via the enhancement in the parameters M , β_1 and γ . Table 3 illustrates the Nusselt number behavior for various influential physical parameters used in this study. Here Rd , δ , Bt and E_1 reveal an enhancing effect over the Nusselt number while Br , E_a , λ_1 , Nt and Nb depicts reverse features. Table. 4 gives the numerical data of Sherwood number in the variations of different influential parameters. Here Sherwood number increases for δ_1 and δ whereas decays for E_a .

7. Concluding remarks

In this research article, the collective features of three dimensional Reiner-Rivlin nanofluid over a rotating disk is explored. Additionally, the flow system is modeled by the considering electrical and activation energies. The key themes are revealed as given below.

- Velocity $g(\eta)$ displays the opposite tendency for higher magnetic parameter M and electric parameter E_1 .
- Thermal field is more dynamic over the increasing values of activation energy E_a , Brownian diffusion parameter Nb and radiation variable Rd .
- Concentration is productive up with improving values of activation energy E_a and thermophoresis parameter Nt , however opposite behavior is noticed for δ and Nb .
- Higher γ leads to additional drag force over the surface of the rotating disk.
- Nusselt number has an enhancing effect for the influential parameters Rd , δ , Bt and E_1 .
- An amplification is noticed in Sherwood number for Biot number Bc and Brownian diffusion variable Nb .
- Entropy optimization is improved for the parameters temperature difference variable α_1 , radiation Rd , Brinkman number Br and electric parameter E_1 .
- The present analysis is only valid for incompressible viscous and electrically conducting fluid and these are the key limitations.

CRedit authorship contribution statement

Refat Ullah Jan: Formal analysis, Visualization, Writing – original draft, Conceptualization, Methodology. Ikram Ullah: Investigation, Supervision, Conceptualization, Writing – original draft. Mohammad

Mahtab Alam: Visualization, Data curation, Writing – original draft. Ali Hasan Ali: Writing – review & editing, Methodology, Software, Validation, Visualization, Project administration.

Declaration of competing interest

The authors declare that they have no known competing financial interests or personal relationships that could have appeared to influence the work reported in this paper.

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