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CASE STUDY



Productivity index of horizontal well in Mishrif formation of Buzurgan oil field – Case study

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ABSTRACT

Horizontal good technology is one of the recent methods in the drilling and exploitation of geological formations in the best and optimal ways, because of the many and comprehensive advantages that these wells enjoy with the most important measurement and prediction index called productivity index. Which is equivalent to several times higher than the vertical well productivity index, if the field is invested by drilling vertical wells only.

The current research focuses on calculating the productivity index by proposing the development point of view of the reservoir formation in the Burgan oil field through the production of oil from the production units approved in the formation (MB21, MC1, MC2) by using of horizontal good technology and comparing it with the value of the productivity index of vertical wells in the same production units.

Well-known published methods adopted in the case of steady state and pseudo steady state were used in the calculations of the productivity index, and by comparison with the standard observed results, it was found that the Joshi method was closer than others in the calculations of the productivity index for both steady and pseudo steady state cases. Then the calculations were completed taking into account all conditions and factors that have a significant role in the value of the calculated productivity index.

The obtained results revealed that PI increases with [well length, isotropy ratio (K_v/K_h), well thickness vs. well length] increase, while it was decreased with [drainage area] increase in the case of steady state conditions. Also, the PI increase with length increase in the case of Pseudo steady state condition for all the studied methods, and both of Kuchuck and Economides methods seem to be close in obtained results, but Economides is the closest one to the reality and importance in application with the present case. Completion configuration has an effluence on the PI, and it is increasing with the increase of well opening to the production for such well length.

Also, all the results indicated that the use of this type of technology in the field development is good and promising, and gave valuable, excellent, and optimistic results for the future production of the field in a profitable manner.

KEYWORDS

productivity index, horizontal well, Mishrif formation, Buzurgan oil field

1. INTRODUCTION

The technology of drilling horizontal wells constituted a qualitative leap in the world of oil engineering, as companies began to compete to use technology and develop it in the direction of increasing production and optimal use of natural resources such as crude oil and natural gas and reducing the costs of invested capital.

Mainly horizontal well drill to increase the production of oil or gas in comparison with vertical wells, and when the decision of both production and reservoir engineers (reservoir management) is pointing towards the development of oil and gas fields by using the horizontal wells technology, then it is necessary to take into consideration the percentage of the productivity of horizontal wells versus the productivity of vertical wells, in addition to the

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properties of both the reservoir and the well as a whole, knowing that this percentage of the productivity was considered to the good pressure is constant.

Also, from the data extracted from this percentage of productivity, we find that the horizontal wells have 2–3 times higher productivity than the vertical wells, and this will certainly be adopted. The length of the drilled horizontal section and the density of perforation areas along the section affect on well productivity.

In the case of such reservoirs where the oil is under potential conditions that make it have one phase (under-saturated), we find that the yield of its wells will be proportional to the value of the pressure drop between the reservoir pressure and the good pressure; this factor of proportionality is represented by the productivity index PI, which is denoted by the letter 'J' and its unit is 'STB/D/Pisa', this parameter quantifies the ability of the reservoir to give up a quantity of oil in barrels per day in exchange for a pressure drop, whereas an inflow performance relationship is a measure of the ability of the formation or layer to produce a certain amount of oil and gas that can be controlled by PI.

It was clear from the studies and researches dealt with or included in this regard that many factors affect the amount of pressure in both layers and the well together, and thus affect the productivity of wells. These factors include, among others, reservoir drainage area, pay zone thickness, reservoir isotropy (Kv/Kh), well length and fluid properties.

Other productive design factors affect the amount of pressure drop, which are related to the nature of the wells' completion, like perforations, partial penetrations, gravel pack as well as damage due to drilling and completions.

Accordingly, it can be considered that the PI is a valuable methodology through which it is possible to predict or extrapolate the performance of productive wells or reservoirs in general.

1.1. Objective of the work

The main objective of this work was to investigate the comparative study of different horizontal well productivity index models for Mishra Formation in the Buzurgan oil field as a case study.

1.2. Methodology

To study the possibility of implementing horizontal wells by calculating the productivity index PI in the Mishrif formation of the Buzurgan oil field according to different published models for both steady and pseudo steady state of a reservoir, this includes the following steps: -

1.2.1. Extracting the necessary field data from technical reports and field information.

1.2.2. Conducting the first step of calculations for the productivity Index PI with the most acceptable and published methods in the case of the steady state, taking into account all factors and variables affecting the calculations. Conducting the second part of calculations for the productivity Index PI with the most acceptable and published

methods in the case of the pseudo steady state, taking into account all factors and variables affecting the calculations.

1.2.3. A comparison of the calculations for both steps with the reality of the situation and the indicator in the field measurements to know the extent of validity and reliability of the calculations and the accuracy of the adopted chosen model in each case, under validation PI model section.

1.2.4. Conducting the conclusions for the research with recommendations.

1.3. Buzurgan oil field

The Buzurgan oil field is located in the South-Eastern part of the Republic of IRAQ, close to the Iran boundary, 40 Km North East of Amara. The oil field was discovered in 1970, and in November 1976 its development was started. The oil field development was carried out by the general organization of south oil – Missan Oil field. Figure 1 shows the geographical location of the Buzurgan oil field, while Fig. 2 shows the formation stratigraphy in the field.

The structure of the field is an elongated fold consisting of two domes north and south, separated by a shallower saddle along the longitudinal axis of the structure. The main reservoir in the field is Mishrif formation, which is composed of three units, which are also divided into layers depending on the difference in the different depositional environmental and petrophysical properties. Among these units, MB21, MC1 And MC2 are better because of their properties and amount of oil reserve.

2. STRATIGRAPHY1

Buzurgan geological structure is composed of Tertiary and Upper cretaceous deposits. Lower deposits were not penetrated. Stratigraphy description is made according to data given in the final geological reports for Buzurgan wells, these reports are specialist for Missan oil company (operator of the field), for review but not for publishing.

2.1. Mishrif formation

The top is characterized by an unconformity. The formation is presented by limestone of white, light-brown, and brown color due to oil stain; it is presented by crystalline to microcrystalline limestone, by soft to medium-hard limestone, recrystallized and chalky in some parts with bioclastic, cavernous and sometimes limestone interbeds (mudstone, wackestone, packstone, grainstones). Thickness is 331–373 m.

The Mishrif formation covered from the top by the al-Khatib formation, where the al-Rumaila formation comes to the bottom, and the total thickness reaches about 340 m. The formation is divided into three main units (MB21, MC1, and MC2), and these units in turn were divided into secondary layers depending on the difference in the rock facies as a result of a change in environmental conditions during sedimentation.

The bottom part of the formation consists of limestone chalk rocks with a semi-basin environment and represents a



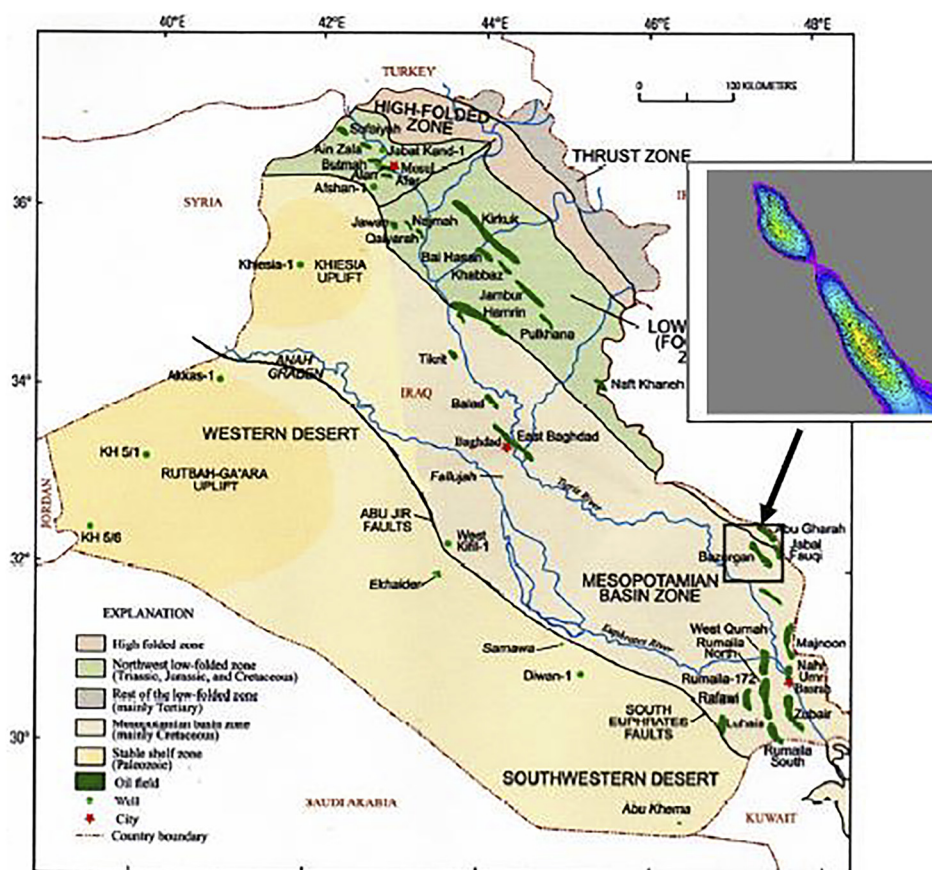


Fig. 1. Location of Buzurgan oil field after ref. [1]

transitional stage between the deep marine environment of Rumaila and the local environment of coral aggregations that represent the middle part of the formation. These agglomerations are of great importance because they have good porosity and permeability and contain good quantities of oil.

The upper part of the formation consists of limestone rocks, which have an environment of tide up, that forms the rock cover of the reservoir.

MB21

It is considered one of the most important formation units, as it has good quantitative properties and contains the highest percentage of oil reserve, and its thickness ranges between 72 and 91 m. The porosity ranges between 13.3 and 17.6% and the permeability rate is less than 10 md. OWC at a depth of 3,875 m in the Northern dome and 3,891 m in the southern dome measured from sea level. The facies in this unit are graded from facies with high porosity and low permeability to shallower facies left in the middle and top of this unit, which are granular rocks deposited in high energy conditions with high initial porosity and high avoidance, in the form of a high production area in this unit.

MC1

The second important formation unit which has a thickness ranges within 61–97 m and porosity of 12.5–17.5% and permeability less than 20 md. The OWC located at depth of 3,994 m in the northern dome while at 3,950.6 m in

the southern dome measured from sea level. Most of the rock unit consists of lagoon facies of low porosity interbedded with wedding Rhodes, which make it reservoir rocks having good properties of primary porosity and permeability.

MC2

The third formation unit has a thickness range of 29–45 m and a porosity of 11–15.8. The OWC is located at depth of 3,982 m in the northern dome while at 3,995 m in the southern dome measured from sea level. Most of the rock units consist of wacky limestone to muddy limestone precipitates in conditions of a slope to the basin, and it is a chalky habit in most parts of it. It is characterized by high porosity and poor permeability, except that the surface of the particle recession may improve the permeability due to the expectation of cracks in it with the presence of some Rhodian clusters.

3. RESERVOIR AND WELL DATA

As mentioned before, the main reservoir in the Buzurgan oil field is Mishrif formation with 206 m thickness, and it is consisting of three productive layers (MB21, MC1, and MC2) which were detailed before. The following table includes the main input data for the calculations of the Productivity index for both MB21 and MC1 layers where the

Age	Formation	Lithology	Description	Symbol
Neocene	Bachitany, upper, Medium, and Lower Fars		Represent by Clay, Shale, anhydrite, some sandstone, Clay shale and White Dolomite	Shale
				Clay
Lower Miocene to Oligocene	Asmari		Limestone, Dolomite and Anhydrite, and Dolomitic shale	Anhydrite
				Sandstone
Cretaceous			Clay, limestone, Clay shale, Sandstone, and Dolomite	Limestone
Turonian to upper Cenomanian	Mishirif		Mainly Limestone and characterized by thin layer on the top, limestone vary from soft to medium and hard (Mudstone, Packstone, Wackstone, Grainstone)	

Fig. 2. Stratigraphy description for Buzurgan structure after ref. [1]

MC@ layer was excluded because of lack of data obtained, in addition to the fact that the layer is characterized by poor physical properties.

4. CALCULATIONS OF PI

4.1. Steady state condition

Under the steady state condition, the reservoir pressure is constant everywhere in a reservoir and this needs a pressure potential to substitute the pressure drops due to production from wells in the reservoir. Joshi [2] explains why this type of solution is more preferred and desirable according to: -

- They are easy to derive analytically
- It is fairly easy to convert results of steady state to either transient or pseudo steady state results by using concepts of expanding of drainage boundary over time and effective good radius and shape factor respectively
- The results of mathematical modeling of steady state can be verified experimentally.

Several solutions are published in the literature to perform and predict the steady state productivity index in a horizontal well, those are: -

4.1.1. Borisove Model [3]

4.1.2. Giger [4]

4.1.3. Joshi Model [2]

4.1.4. Renard and Dupuy model [5]

All the mathematical models are explained in detail within Appendix A.

4.2. Pseudo steady state

Under pseudo steady condition, the good boundary drainage area was felt by pressure drop due to well production and made the fluid at its side moving toward the well. Whatever the shape of the drainage area (depends on permeability isotropy), when the pressure disturbance due to well production reaches all the boundaries, the pseudo steady state begins, so the time required for that is ($t = 948 \phi \mu c t_{re2}/k$).

Also, in this condition state, the reservoir must have closed boundaries and there should be no flow across it. The pseudo steady state solution is suitable for predicting well performance in the depletion stage of the reservoir, and productivity index under this condition can be performed within average reservoir pressure that was estimated by well testing (build up or drawdown). Some of the methods were published in the literature to calculate the pseudo steady state productivity index for horizontal wells for single-phase flow with assumptions, like: -

- The reservoir is assumed bounded in all directions
- The horizontal well was arbitrarily located within a rectangular bounded drainage area

Joshi [2] explained three methods of PI calculation according to their differences in well consideration, those are: -

- Method I, assumes the well as infinite conductivity
- Method II, assumed a uniform flux boundary condition
- Method III, uses an approximate infinite conductivity with constant wellbore pressure (averaging pressure values of uniform flux along the well length).

There are four pseudo steady state equations published in literatures to measure the productivity index of horizontal oil wells, these are: -

4.2.1. Joshi Model [2]

4.2.2. Babu and Odeh Model [6]

4.2.3. Kuchuk model [7]

4.2.4. Economides Model [8]

All the mathematical models are explained in detail within Appendix A.

Calculations of PI with different models. The general input data for this section were taken from ref. [9], and according to the different petrophysical properties, the main reservoir in the field is Mishrif formation which was divided into 3 main productive Layers (MB21, MC1, MC2) – Table 1 includes the important data for each layer that were used with the PI models and correlations; Table 2 shows the results of PI calculations according to the steady state methods explained in the previous section as a base case.

While Tables 3–10, shows the final calculation results in regard to different parameters that affect PI in each model.

Table 1. Reservoir, fluid and well data

Layer	Reservoir Data	Fluid Data	Well Data
MB21	Kh = 10 md Kv = 10 md H = 81.5 m Tres = 235 Pres = 6,128.7 Psia	$\mu_o = 1.15661$ c.p $B_o = 1.3825$ RB/STB	L = 1,000 ft Rw = 0.365 ft Reh = 1,640 ft A = 194 acres
MC1	$\phi = 15\%$ Kh \leq 20 md Kv \leq 20 md H = 79 m Tres = 235 Pres = 6,128.7 Psia	= =	= =

Table 2. Results of the PI with different methods. (Base Case)

PI - Method	Pi – STB/D/Psia
Borisove Model	3.754
Joshi Model	13.763
Gigers Model	3.783
Renard and Dupuy Model	3.754

For MB21 formation layer.

a. Effect of horizontal well length (Kv/Kh = 1.0)

Table 3. Effect of horizontal well length

PI - Method	Horizontal Well Length			
	1,000 ft	1,500 ft	2,000 ft	2,500 ft
Borisove Model	3.754	5.095	6.49	8.034
Joshi Model	13.763	15	17.547	21.129
Gigers Model	3.783	5.223	6.905	9.251
Renard and Dupuy Model	3.754	5.092	6.475	7.978

b. Effect of an isotropy (Kv/Kh)

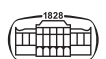
Table 4. Effect of an isotropy

Well Length - Ft	PI Method	Kv/Kh				
1,000		0.1	0.25	0.5	0.75	1.0
	Borisove Model	3.754	3.754	3.754	3.754	3.754
	Joshi Model	—	56.426	20.832	15.856	13.763
	Gigers Model	11.963	7.566	5.35	4.368	3.783
	Renard and Dupuy Model	3.754	3.754	3.754	3.754	3.754
1,500	Borisove Model	5.095	5.095	5.095	5.095	5.095
	Joshi Model	—	33.911	19.996	16.612	15
	Gigers Model	16.515	10.445	7.386	6.031	5.223
	Renard and Dupuy Model	5.096	5.096	5.096	5.096	5.092
2,000	Borisove Model	6.49	6.49	6.49	6.49	6.49
	Joshi Model	277.227	34.551	22.511	19.192	17.547
	Gigers Model	21.835	13.809	9.765	7.973	6.905
	Renard and Dupuy Model	6.475	6.475	6.475	6.475	6.475
2,500	Borisove Model	8.034	8.034	8.034	8.034	8.034
	Joshi Model	222.3	40.268	26.845	23.035	21.129
	Gigers Model	29.26	18.503	13.083	10.683	9.251
	Renard and Dupuy Model	7.978	7.978	7.978	7.978	7.978

c. Effect of well thickness Vs. well length

Table 5. Effect of well thickness Vs. well length

Well Length - Ft	PI Method	0.3	0.5	1.0
1,000				
	Borisove Model	1.639	2.442	3.754
	Joshi Model	2.1313	4.064	13.763
	Gigers Model	1.658	2.466	3.783
	Renard and Dupuy Model	1.639	2.441	3.754
1,500				
	Borisove Model	2.132	3.221	5.095
	Joshi Model	2.664	4.963	15
	Gigers Model	2.208	3.324	5.223
	Renard and Dupuy Model	2.131	3.218	5.092
2,000				
	Borisove Model	2.67	4.056	6.49
	Joshi Model	3.275	6.0474	17.547
	Gigers Model	2.909	4.384	6.905
	Renard and Dupuy Model	2.661	4.044	4.75
2,500				
	Borisove Model	3.604	5.0	8.034
	Joshi Model	4.508	7.361	21.131
	Gigers Model	4.379	5.991	9.252
	Renard and Dupuy Model	3.57	4.965	7.978



d. Effect of drainage area Vs. an isotropy (well length = 1,000 ft)

Table 6. Effect of drainage area Vs. an isotropy

Drainage area - acres	PI Method				
50		0.25	0.5	0.75	1.0
	Borisove Model	4.781	4.781	4.781	4.781
	Joshi Model	—	—	162.241	63.474
	Gigers Model	10	7.063	5.767	5
	Renard and Dupuy Model	4.774	4.774	4.774	4.774
100	Borisove Model	4.194	4.194	4.194	4.194
	Joshi Model	—	49.706	28.424	22.336
	Gigers Model	8.535	6.035	4.928	4.268
	Renard and Dupuy Model	4.193	4.193	4.193	4.193
150	Borisove Model	3.914	3.914	3.914	3.914
	Joshi Model	145.35	26.911	19.146	16.178
	Gigers Model	7.91	5.593	4.567	3.955
	Renard and Dupuy Model	3.913	3.913	3.913	3.913
200	Borisove Model	3.736	3.736	3.736	3.736
	Joshi Model	52.597	20.287	15.539	13.523
	Gigers Model	7.528	5.323	4.346	3.764
	Renard and Dupuy Model	3.736	3.736	3.736	3.736
250	Borisove Model	3.609	3.609	3.609	3.609
	Joshi Model	35.166	17.031	13.554	12
	Gigers Model	7.259	5.133	4.191	3.629
	Renard and Dupuy Model	3.609	3.609	3.609	3.608

Formation layer (MC1).

a. Effect of horizontal well length (Kv/Kh = 1.0)

Table 7. Effect of well length

PI - Method	Horizontal Well Length - Ft			
	1,000	1,500	2,000	2,500
Borisove Model	7.389	10.012	12.747	15.776
Joshi Model	25.543	28.142	33.05	39.837
Gigers Model	7.446	10.267	13.573	18.204
Renard and Dupuy Model	7.388	10.01	12.717	15.67

b. Effect of an isotropy (Kv/Kh)

Table 8. Effect of an isotropy

Well Length - Ft	PI Method	Kv/Kh				
1,000		0.1	0.25	0.5	0.75	1.0
	Borisove Model	7.389	7.389	7.389	7.389	7.389
	Joshi Model	—	83.418	37.107	29.069	25.543
	Gigers Model	23.547	14.893	10.531	8.598	7.446
	Renard and Dupuy Model	7.388	7.388	7.388	7.388	7.388
1,500	Borisove Model	10.012	10.012	10.012	10.012	10.012
	Joshi Model	155.306	58.278	36.643	30.933	28.142
	Gigers Model	32.467	20.534	14.519	11.855	10.267
	Renard and Dupuy Model	10.01	10.06	10.01	10.01	10.01
2,000	Borisove Model	12.747	12.747	12.747	12.747	12.747
	Joshi Model	254.187	60.959	41.589	35.917	33.05
	Gigers Model	42.92	27.145	19.194	15.672	13.573
	Renard and Dupuy Model	12.717	12.717	12.717	12.717	12.717



c. Effect of well thickness Vs. well length

Table 9. Effect of well thickness Vs. well Length

Well Length - Ft	PI Method			
1,000		0.3	0.5	1.0
	Borisove Model	3.195	4.774	7.389
	Joshi Model	4.1097	7.788	25.544
	Gigers Model	3.2313	4.822	7.446
	Renard and Dupuy Model	3.195	4.773	7.388
1,500	Borisove Model	4.153	6.291	10.011
	Joshi Model	5.140	9.529	28.142
	Gigers Model	4.3	6.494	10.267
	Renard and Dupuy Model	4.149	6.286	10.01
2,000	Borisove Model	5.197	7.918	12.747
	Joshi Model	6.323	11.628	33.049
	Gigers Model	5.666	8.565	13.572
	Renard and Dupuy Model	5.181	7.895	12.717
2,500	Borisove Model	7.018	9.78	15.776
	Joshi Model	8.698	14.15	39.836
	Gigers Model	8.538	11.71	18.204
	Renard and Dupuy Model	6.953	9.69	15.67

Pseudo steady state – PI. In accordance with this state of PI calculations, it seems suitable and well applicable for the Buzurgan oil field, because the production history and policy of the field operations and monitoring revealed that the field produces under depletion drive strategy since the first period of production, as well as the calculations of this section proved that clearly. Table 11 presents the results of the PI calculations according to the pseudo steady state methods that were presented before.

Table 11. Pseudo steady state productivity index

Method	PI – (STB/D/Psia)		
	1,000 - Ft	1,500 - Ft	2,000 - Ft
Mutalik et al.	4	6.4	8.68
Babu and Odeh	0.491	0.623	0.754
Kuchuck	5.049	6.752	8.986
Economides	5.564	8.921	13

It is clear from the results of Table 11 that an increase in the good length led to an increase in the productivity index for each psi pressure drop in the reservoir for all the methods, but the method of **Economides** seems to be the suitable one to mimic the production from the field in comparison with the other methods and observed data.

5. VALIDATION OF PI MODELS

d. Effect of drainage area Vs. an isotropy (well length = 1,000 ft)

To make validation for the PI calculations with different Published models under the production circumstances and restrictions (either steady state or pseudo steady state), one can use the observed data for comparison purposes or with

Table 10. Effect of drainage area Vs. an isotropy

Drainage area - acres	PI Method				
50		0.25	0.5	0.75	1.0
	Borisove Model	9.451	9.451	9.451	9.451
	Joshi Model	—	—	198.789	102.266
	Gigers Model	19.761	13.973	11.409	9.88
	Renard and Dupuy Model	9.435	9.435	9.435	9.435
100	Borisove Model	8.271	8.271	8.271	8.271
	Joshi Model	—	79.698	50	40.408
	Gigers Model	16.835	11.904	9.719	8.417
	Renard and Dupuy Model	8.267	8.268	8.267	8.267
150	Borisove Model	7.708	7.708	7.708	7.708
	Joshi Model	156.376	46.826	34.713	29.801
	Gigers Model	15.579	11.017	8.995	7.789
	Renard and Dupuy Model	7.706	7.706	7.706	7.706
200	Borisove Model	7.352	7.352	7.352	7.352
	Joshi Model	79.031	36.213	28.517	25.117
	Gigers Model	14.816	10.476	8.554	7.408
	Renard and Dupuy Model	7.352	7.352	7.352	7.352
250	Borisove Model	7.099	7.099	7.099	7.099
	Joshi Model	57.109	30.796	25.048	22.386
	Gigers Model	14.279	10.096	8.244	7.139
	Renard and Dupuy Model	7.098	7.098	7.098	7.098



simulation results. Herewith our case of horizontal wells production from Mishrif formation in Buzurgan field, no published data were found in the literature, but as a guess from the production of vertical wells and physical properties and by using an analog of another field in the same area in the same formation, one can estimate the well PI range for these types of wells, which are in between 13 and 14 STB/D/Psia, therefore from the base case results, Joshi [2] was the proper method for calculations of PI under steady state condition, while the **Economides** method was suitable for the calculation of PI under pseudo steady state condition.

6. COMPLETION CONFIGURATION ON PRODUCTIVITY INDEX –PI

This issue discusses the completion configuration effect on well productivity index through studding of skin damage types, as it is found in the literatures [10], there are three types of damage as follows:

1. Skin due to perforation, S_{PF}
2. Skin due to penetration, S_p
3. Skin due to crush zone permeability, S_C

Here, the damage caused by the penetration of the well to the formation layers will be discussed. If the penetration is complete, then the amount of damage is considered equal to zero ($S_p = 0$), while if the penetration is partial, it will be calculated and discussed according to a method of Brons and Marting method [10]. Oaken E. and Oloro J [11], presented a scenario to apply the method of Brons and Martin as follows: -

The method uses 3 types of configuration form for horizontal wells, namely: -

- (a) Well producing from the top (or bottom) of the formation, named as case I
- (b) Well only producing from the central section, named as case II
- (c) Well with N intervals open to production (five [5] open intervals, named as case III

For three completion configurations forms of the producing wells, using any of the given configurations, the pseudo skin can be calculated due to partial penetration through which we obtain the productivity index for each case.

The pseudo-skin factor was calculated for both layers MB21 and MC1 of Mishrif Formation, using of Brons and Marting method for the case of partial penetration which results in skin productivity index, the results are presented in Table 12.

7. RESULTS AND DISCUSSION

The obtained results from the calculations of PI for horizontal well incorporated within the Mishrif formation in

Table 12. Productivity Index for MB21 and MC1 layers of Mishrif formation due to penetration ratio and pseudo skin for partially completion wells

Case	b'	S_p	Jh (STB/D/Psia)
Layer MB21 (h = 267.4 ft)			
I	0.2	18.8024	1.704
	0.4	7.5915	3.437
	0.6	3.303	5.6293
	0.8	1.1512	8.2772
II	0.2	16.0298	1.9464
	0.4	6.552	3.7958
	0.6	2.8407	6.0446
	0.8	0.9778	8.6031
III	0.2	9.5921	2.9092
	0.4	4.1376	5.01
	0.6	1.7677	7.294
	0.8	0.5755	9.468
Layer MC1 (h = 259.2 ft)			
I	0.2	18.678	1.666
	0.4	7.545	3.367
	0.6	3.282	5.529
	0.8	1.1434	8.157
II	0.2	15.9052	1.9055
	0.4	6.5051	3.722
	0.6	2.8199	5.943
	0.8	1.1434	8.484
III	0.2	9.4675	2.862
	0.4	4.901	4.9286
	0.6	1.747	7.1924

Buzurgan oil field were subdivided into two main categories (steady state and unsteady state calculations) with different parameters that affected the PI of horizontal wells, which are mentioned for each layer of the formation. Tables 2–11 show these results. A special calculation code program was done under MATLAB environment to facilitate and ease changes with those parameters of calculations of each case within each layer.

1. **Steady state condition.** It was shown that the results have been the same trend effect for each parameter on calculations of PI for both MB21 and MC1 layers, except for MC2, because of the lack of data obtained with some real field and properties data.

1.a. all the calculations in Tables 3–7 refer to increase in the PI with the increase of good length, and for all methods especially for the regions in layer MB21 with similar values or nearby of K_v and K_h , and this is true in coincidence with the effect of this parameter in PI equations.

1.b. Joshi and Giger's models reveal that the PI improves its values toward the increasing of heterogeneity in layer even though Joshi failed with ($K_v/K_h = 0.1$), while both of Borisove and Renard and Dupuy models could not sense these changes of Isotropy parameter.

1.c. Also, in this section, all the methods have shown the effect and importance of changing the well length with



different values of good thickness, this type of results shows how much incremental gain is in productivity with a thick or thin layer of reservoir. A horizontal well results in more produce from thin layers of the reservoir than a thick one, and this is an attribute to wellbore exposure to the reservoir layer.

1.d. With the fixing of good length, variation of drainage area with different values of isotropy, Joshi and Giger methods reveal encouraging results for each drainage with limitations, because of isotropy within formation layer, and this is clear when the drainage area is less than the drainage area of the Base case.

2. Pseudo steady state conditions

2.a. It seems from the results shown in Table 11, that all the methods have an increase the PI with the increasing of well length in both of MB21 and MC1 layers of Mishrif formation [12].

2.b. Also it seems that both of Mutalik et al. Kuchuck methods have similar values, while Babu and odel is far off in its PI from the other methods and this is due to the consideration of methodology and consideration of parameters in calculations of the methods.

2.c. Kuchuck and Economides methods are considered close in the results obtained from the calculations, and they are closer and more acceptable within the actual reality, and for the lengths close to them in the field.

3. Completion configuration

3.a. The results obtained in this section of the calculations showed that they are close and for both layers of MB21 and MC1 and for the various forms or scenarios taken to complete the horizontal wells.

According to the completion configuration and partial penetration well, as seen from the results of calculation using Brons and Martin method, the productivity index of horizontal well gets better and more valuable with increasing the (hp/h) values, in addition to that, the case III in each layer turned out to be a better choice for completion configuration, because it exposes more formation parts to the well and increasing the exposure production area with the well along the horizontal section that means increasing the productivity index, then increasing the horizontal good production.

4. From the overall calculation results, it seems the method of forecasting and calculations related to PI. It is good evidence of the production chance of commercial quantities of oil and gas in its reservoirs, where the geological and geochemical indications and exploration processes indicated the presence of commercial quantities of hydrocarbon aggregates in the field [13]. These indications used in the oil fields are the relationship between iodine and petroleum systems, the usage of iodine hydro geochemical and pedo-geochemical methods in petroleum exploration and production.
5. As long as the technology of horizontal wells has been widely applied in oil and gas fields and is considered one of the most promising technologies for the development

and valorization of oil and gas fields, there are many regions in the world that are considered among the most promising and strategically important at the political, economic and geological levels, which are characterized by a distinct geographical location and have distinct oil fields, that were rich in hydrocarbon aggregates and in excellent reserves, for example the Central Asian region, which has become one of the energy hubs in the world to help the countries to stand out as a significant stable and sustainable source of energy in the region with great resources of supply and low domestic demand [14]. These regions really need such applications (horizontal wells) in the field of production and field development.

8. CONCLUSIONS

1. Increasing of productivity index with increasing of the horizontal well lengths with different values of heterogeneity described by isotropy (K_v/K_h) values.
2. Some methods of PI steady state failed to sense the PI values in some regions of the field.
3. The PI values affected by drainage area, which reveal positive proportionality with the amount of heterogeneity, and for some of the methods used.
4. Regarding the productivity index for the pseudo steady state case, increasing of the well length leads to an increase in the productivity index.
5. Increasing of open intervals to the production leads to an increase in the productivity index of the horizontal well.

NOMENCLATURE

K_h	Horizontal permeability - md ($K_h = \sqrt{K_y/K_x}$)
K_v	Vertical permeability - md
Δp	Pressure difference - Psia
μ_o	Oil viscosity - cp
B_o	Oil formation volume factor - bbl/STB
R_{eh}	Horizontal well drainage radius - ft
R_w	Well radius - ft
H	Layer thickness - ft
L	Well length - ft
Q_h	Horizontal well flow rate - STB/d
J_h	Horizontal well productivity index (PI) - STB/D/Psia
A	Half major axis of drainage ellipse - ft
P_{wd}	Dimensionless inflow pressure
S_m	Mechanical skin factor
S_i	Skin factor of an infinite-conductivity, fully penetrating fractures of length L
S_{cah}	Shape - related skin factor
C'	Shape factor conversion constant = 1.386
X_e, Y_e	Dimensions of rectangular drainage area - ft



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Appendix A

1- Steady state PI models

Borisov

$$Q_h = \frac{2\pi h \Delta p k_h / (\mu_o B_o)}{\ln \left[\left(\frac{4r_{eh}}{L} \right) \right] + (hL) \ln \left[\frac{h}{2\pi r_w} \right]}$$

Giger

$$Q_h = \frac{2\pi h \Delta p k_h / (\mu_o B_o)}{\left(\frac{L}{h} \right) \left(\frac{1 + \sqrt{1 - \left[\frac{L}{2r_{eh}} \right]^2}}{\left[\frac{L}{2r_{eh}} \right]} \right) + \ln \left[\frac{h}{2\pi r_w} \right]}$$

Renard and Dupuy

$$Q_h = \frac{2\pi h \Delta p k_h}{(\mu_o B_o)} \left[\frac{1}{\cosh^{-1}(x) + \left(\frac{h}{L} \right) \ln \left[\frac{h}{2r_{eh}} \right]} \right]$$

$$X = 2a/L$$

Joshi

$$Q_h = \frac{2\pi h \Delta p k_h / (\mu_o B_o)}{\ln \left[\frac{a + \sqrt{a^2 - (0.5)^2}}{\left(\frac{L}{2} \right)} \right] + \left(\frac{h}{L} \right) \ln \left[\frac{h}{2r_w} \right]}$$

$$a = \left(\frac{L}{2} \right) \left[0.5 + \sqrt{0.25 + \left(\frac{2r_{eh}}{L} \right)^4} \right]$$

2- Pseudo steady state PI models

Joshi Model [2].

Method I

$$J_h = \frac{0.00708 K h / [\mu_o B_o]}{\ln \left(\frac{r_{e'}}{r_w} \right) - A' + S1 + Sm + Scah - C' + Dq}$$

$$r_{e'} = \sqrt{A/\pi}$$

Methode II

$$J_h = \frac{0.00708 (2X_e) (\mu_o B_o) \sqrt{K_v K_h}}{\ln \left(\frac{A}{r_w} \right) + \ln Ch - 0.75 + Sr}$$

$$\ln Ch = 6.28 \left(\frac{2y_e}{h} \right) \sqrt{\frac{K_h}{K_v}} \left[\frac{1}{3} - \left(\frac{Y_w}{2Y_e} \right) + \left(\frac{Y_w}{2Y_e} \right)^2 \right]$$

$$- \ln \left[\sin \left(180 \frac{Z_w}{h} \right) - 0.5 \ln \left[\left(\frac{2Y_e}{h} \right) \sqrt{\frac{K_v}{K_h}} \right] - 1.88 \right]$$

$$\text{Case 1 : } 2 \frac{Y_e}{K_v} \geq 1.5 \frac{X_e}{\sqrt{K_x}} \gg 0.75h/\sqrt{K_v}$$



$$\text{Case 2 : } 2 \frac{X_e}{K_x} \geq 2.66 \frac{Y_e}{\sqrt{K_y}} \gg 1.33h/\sqrt{K_v}$$

Case 1

$$S_R = PXY + PXY'$$

$$PXYZ = \left[\frac{2Xe}{L} - 1 \right] \left[\ln \left(\frac{h}{r_w} \right) + 0.25 \ln \left(\frac{K_y}{K_v} \right) - \ln \left(\sin \frac{180 Z_w}{h} \right) - 1.84 \right]$$

$$PXY' = \left(\frac{2(X_e)^2}{hl} \right) \left(\sqrt{\frac{K_y}{K_v}} \right) [F(x) + 0.5 \{ (fy1 - fy2) \}]$$

$$X = \frac{L}{4Xe} \quad Y1 = \frac{4Xe + L}{4Xe} \quad Y2 = \frac{4Xe - L}{4Xe}$$

$$F(x) = -x[0.145 + \ln(x) - 0.137(x^2)]$$

$$F(y) = (2 - Y)[0.145 + \ln(2 - Y) - 0.137(2 - Y)^2]$$

$$Y = Y1 \text{ or } Y2$$

Case 2

$$S_R = PXYZ + PY + PXY$$

$$Sx = \ln \left[\left(\frac{\pi r_w}{h} \right) \left(1 + \sqrt{\frac{K_v}{K_h}} \right) \sin \left(\frac{\pi Z_w}{h} \right) - \sqrt{\frac{K_h}{K_v}} \left(\frac{2h}{L} \right) \left[\frac{1}{3} - \left(\frac{Z_w}{h} \right) + \left(\frac{Z_w}{h} \right)^2 \right] \right]$$

Babu and Odeh Model [6].

$$Jh = \frac{0.703 * b * \sqrt{K_x K_z} * \mu g * z}{T(\ln(CH * A[*rw] - 0.75 + SR))}$$

Kuchuk model [7].

$$Jh = \frac{0.703 * KH * h * \mu g * z}{T(PwD + SM*)}$$

$$PwD = \frac{h}{2L} \sqrt{\frac{K_x}{K_z}} \left(\ln \frac{8h}{\pi r_w} \cot \left(\frac{\pi Z_w}{2h} \right) + \left(\frac{Z_w - h}{L} \right) \sqrt{\frac{K_x}{K_z}} \right)$$

$$Sm = \left(\frac{2\pi L \sqrt{K_y K_z}}{\mu q} \right) \Delta Ps$$

$$Sm^* = \frac{h}{2L} \sqrt{\frac{K_x}{K_z}} Sm$$

Economides Model [8].

$$J = \frac{0.73 * Kavg * Xe * \mu * z}{T \left(PD + \frac{Xe}{2\pi L} \right) \sum S}$$

$$PD = \frac{Xe CH}{4\pi h} + \frac{Xe}{2\pi L} Sx$$

$$Sx = \ln \left(\frac{h}{2\pi r_w} \right) - \frac{h}{6L} + Se$$

$$Se = \frac{h}{L} \left(\left(\frac{2 * Z_w}{h} \right) - 0.5 \left(\frac{2 * Z_w}{h} \right)^2 - \ln \left(\sin \left(\frac{\pi * Z_w}{h} \right) \right) \right)$$